

Different ways of measuring texture gradients by diffraction

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Deformation processes are generally complicated due to frictional effects and flow instabilities causing texture gradients!

- **tension**
necking (+ shear banding (SB))
- **compression**
friction at anvils (+ SB)
- **torsion**
per se strain gradient (+ SB)
- **bending**
per se change from tension to compression + SB
- **wire drawing, extrusion**
friction at die walls (+ SB)
- **rolling**
friction at rolls (+ SB)
- **equal channel angular pressing (ECAP)**
friction at channel walls (+ SB)

texture ↔ properties ↔ property gradient

Requirements for measuring specific texture gradients by diffraction

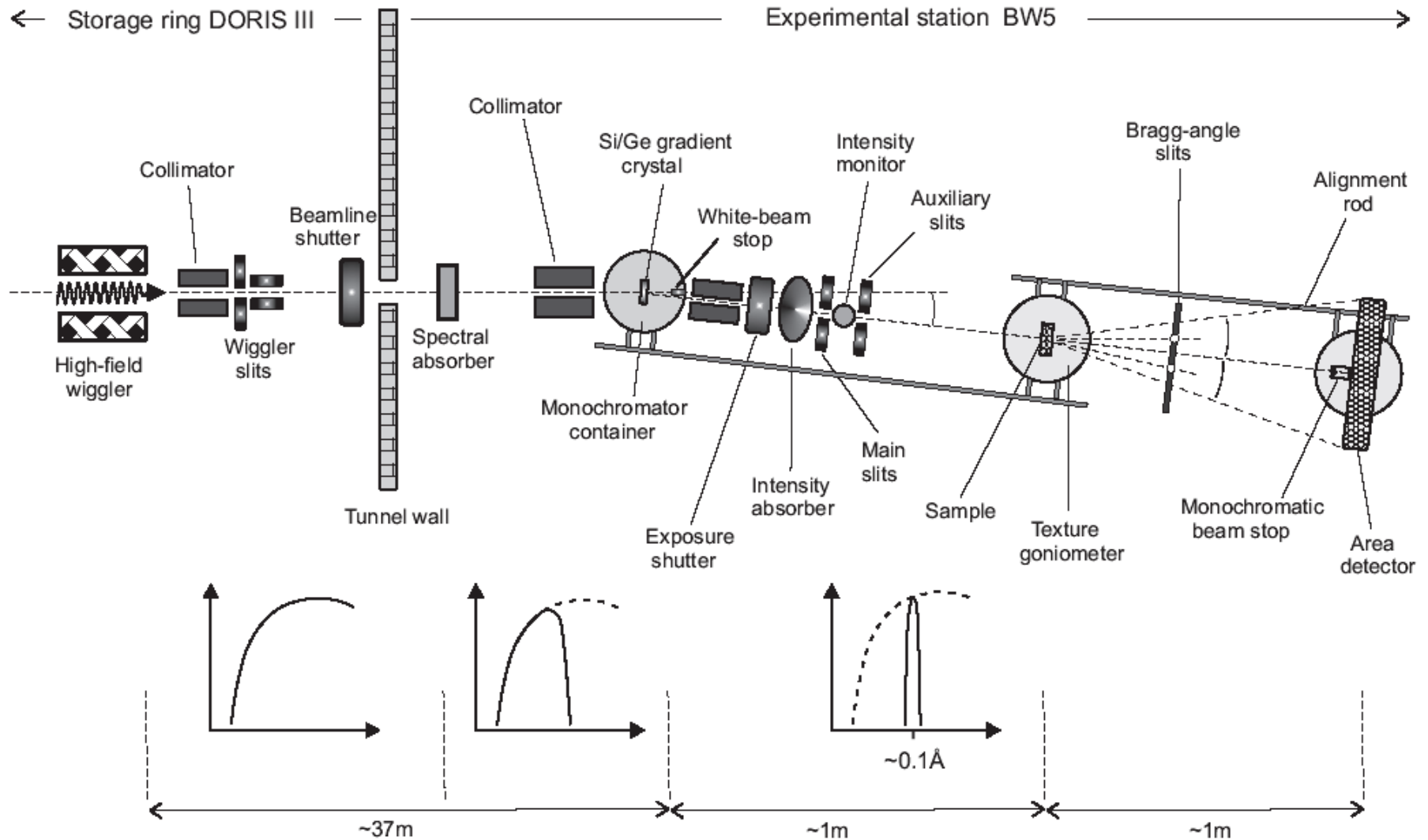
Radiation		Beam size	Grain statistics
	$d_{1/2}$		
X-rays (soft)	1-50 μm	cm^2	
X-rays (hard)	>1 mm	mm^2	
neutrons	>1 cm	cm^2	
electrons	< 1 μm	100 nm^2	problem

Examples:

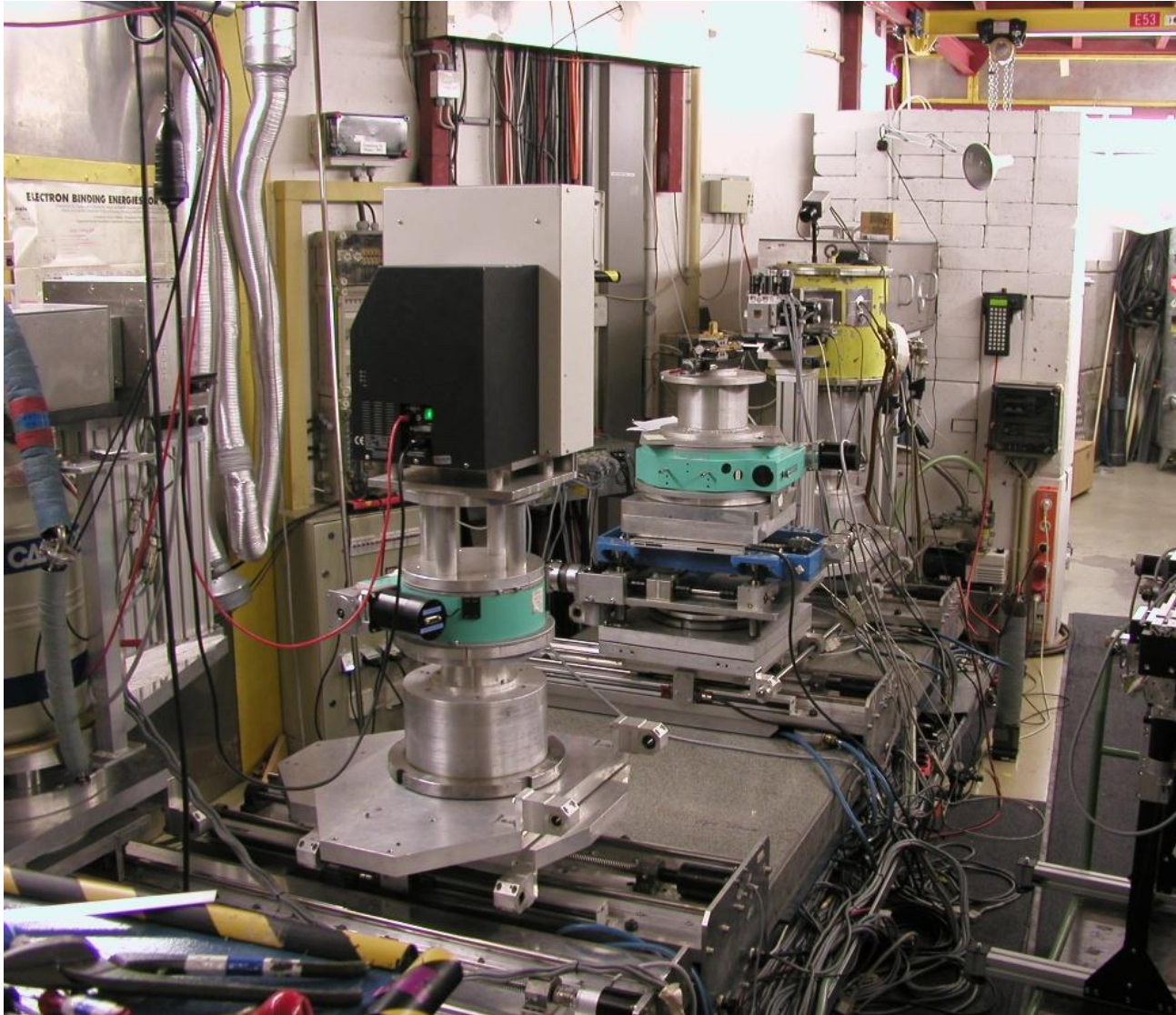
Texture gradient in ECAP by diffraction of synchrotron radiation

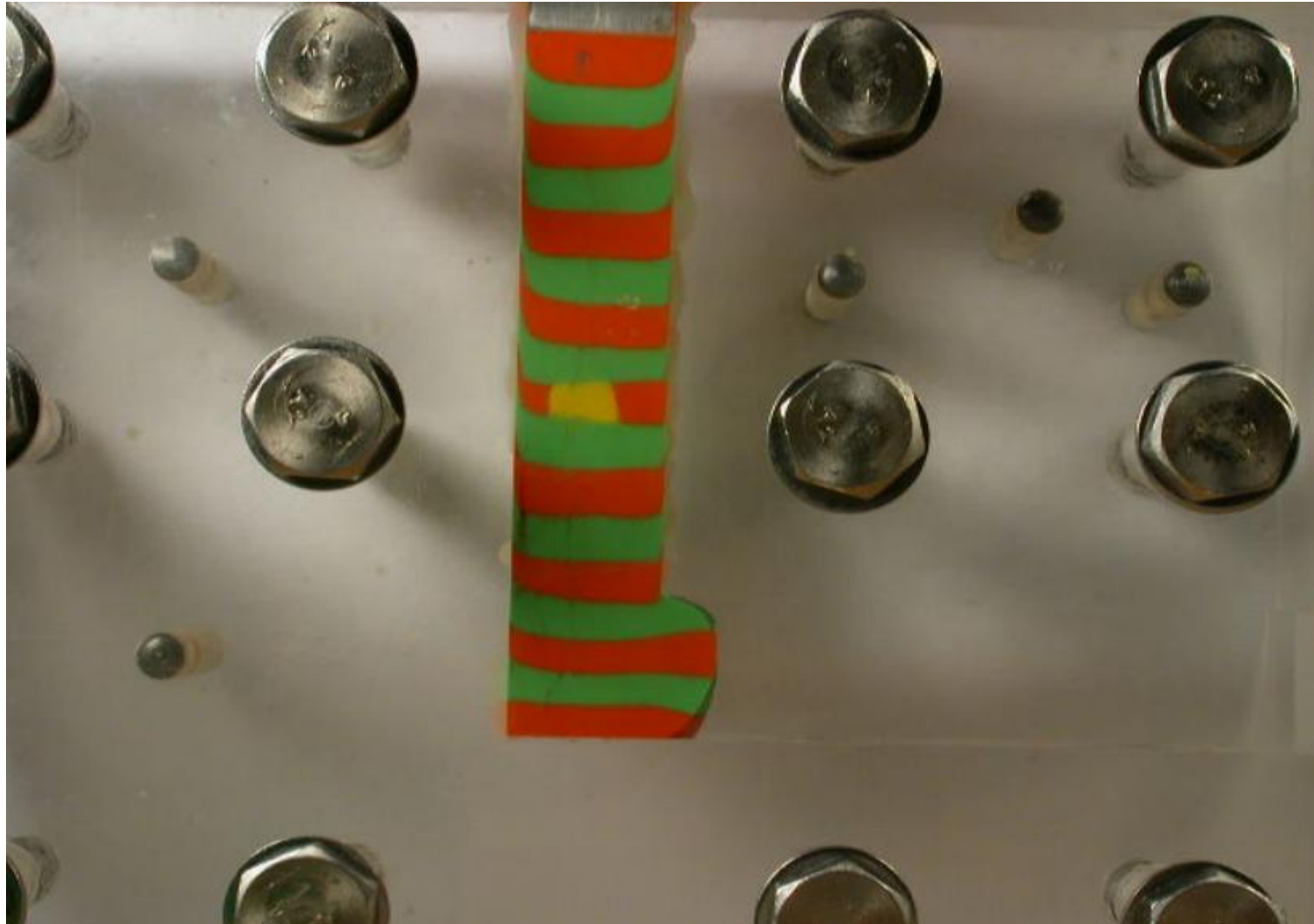
Texture gradient in HPT nanomaterial by X-ray microdiffraction

Experimental station BW 5 at HASYLAB



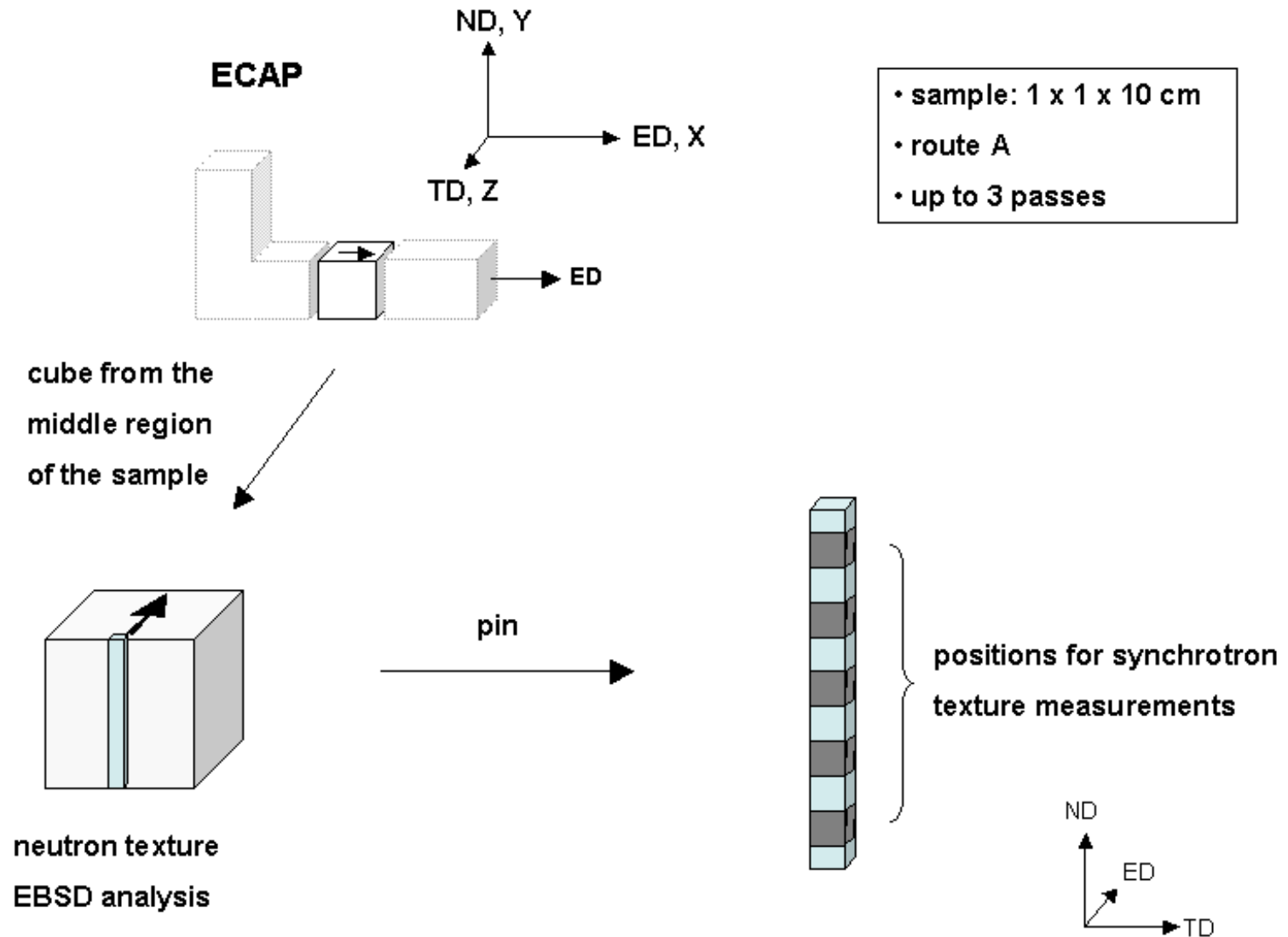
Diffraction of synchrotron radiation at BW5, DESY/HASYLAB in Hamburg



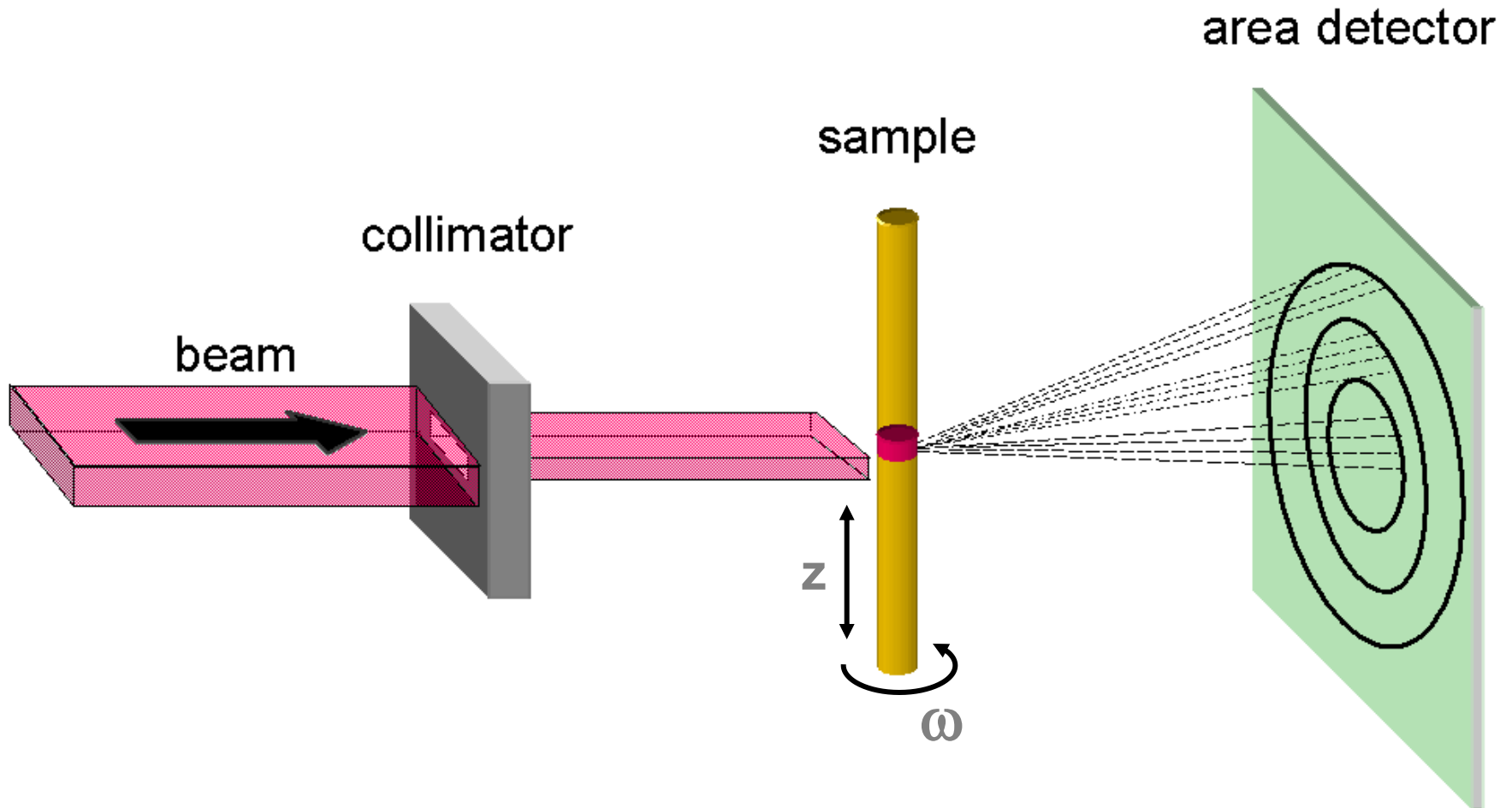


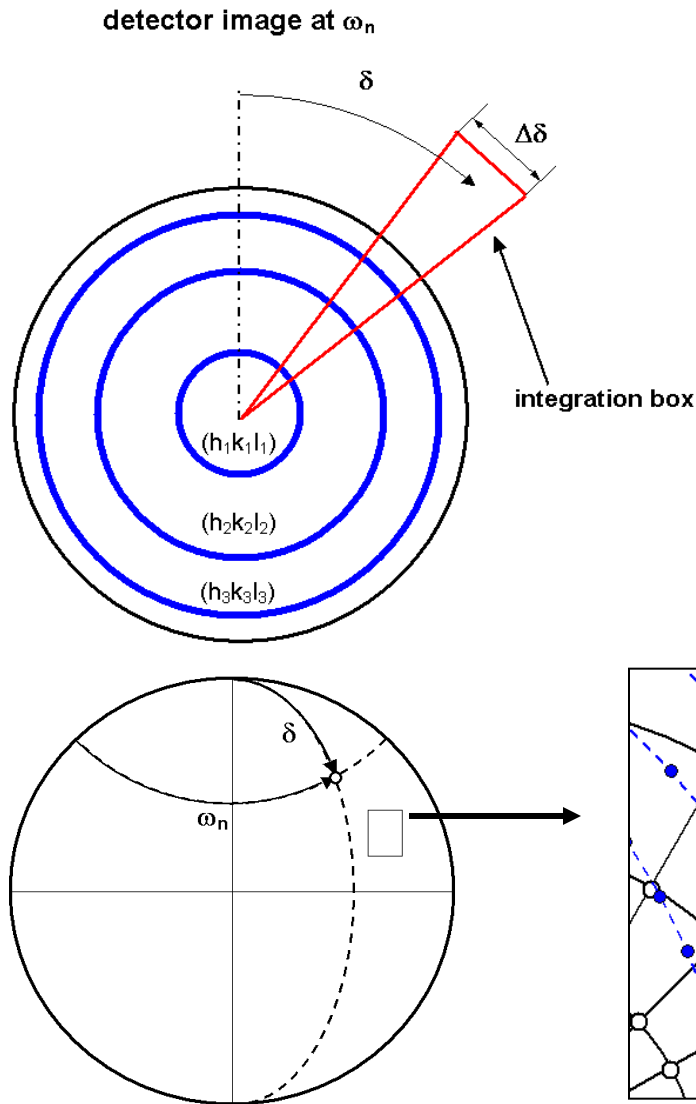
plasticine in ECAP die

ECAP: sampling

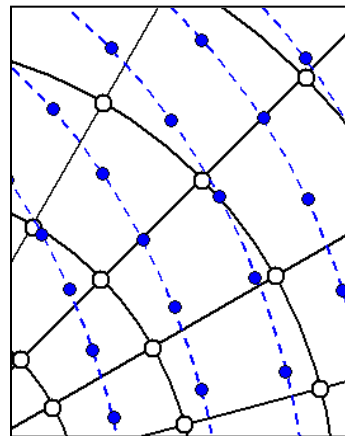


Texture measurements with synchrotron radiation

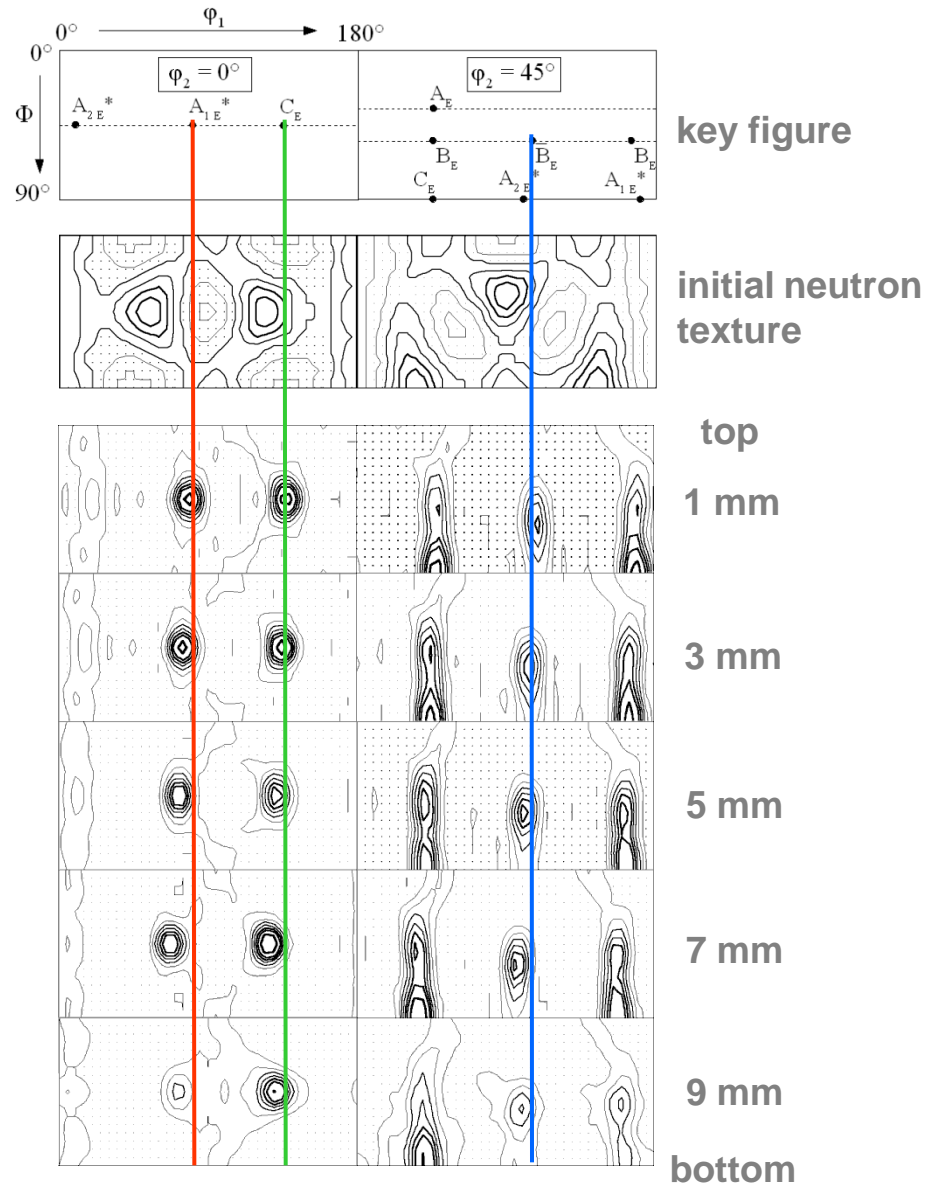




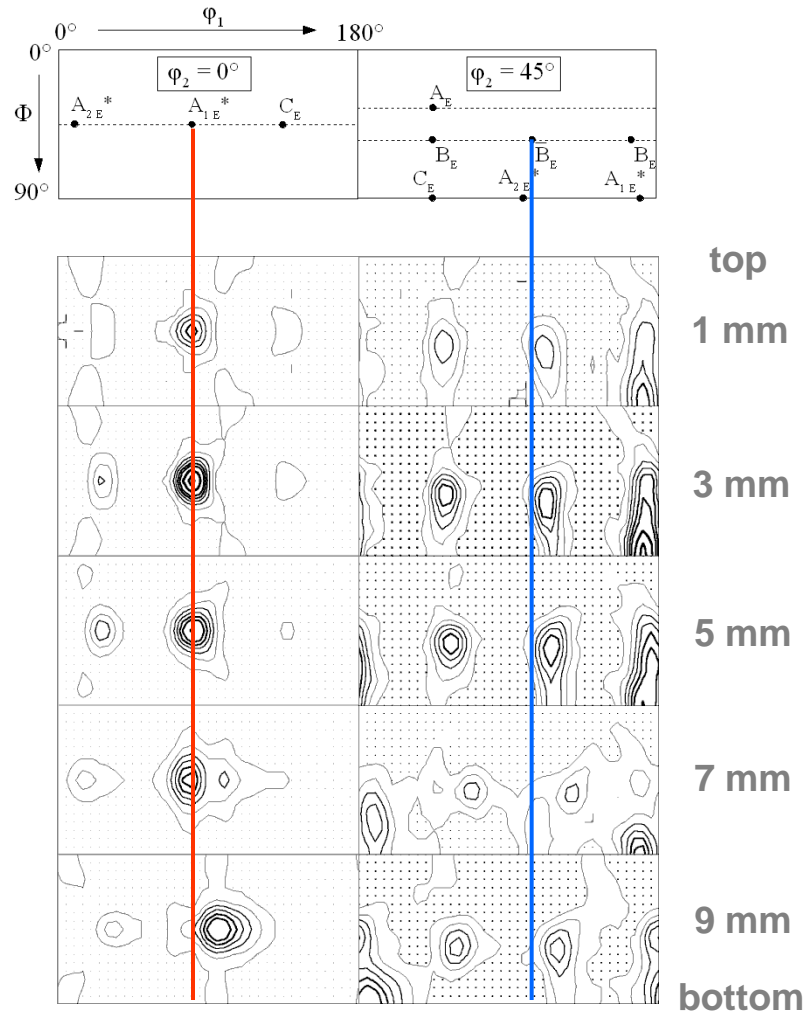
- read out of intensities along each Debye-Scherrer ring in steps of 5°
- intensity values are copied into the corresponding pole figure on an irregular grid
- interpolation on a regular $5^\circ \times 5^\circ$ grid



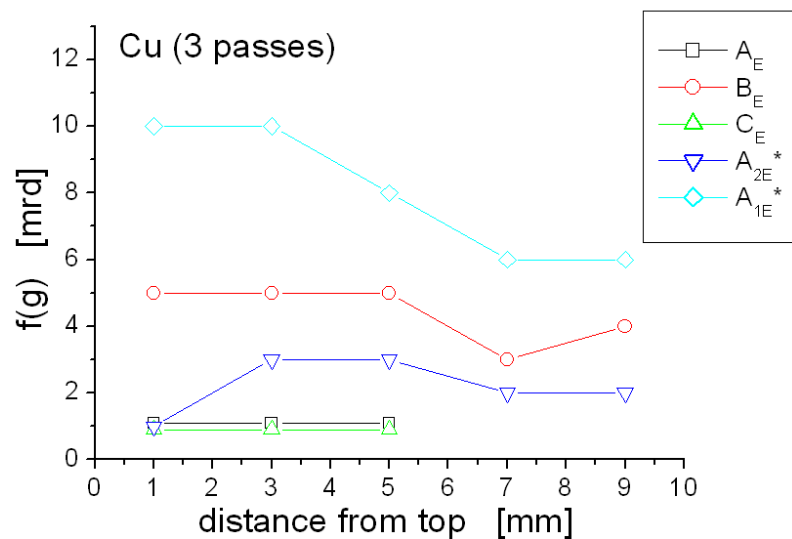
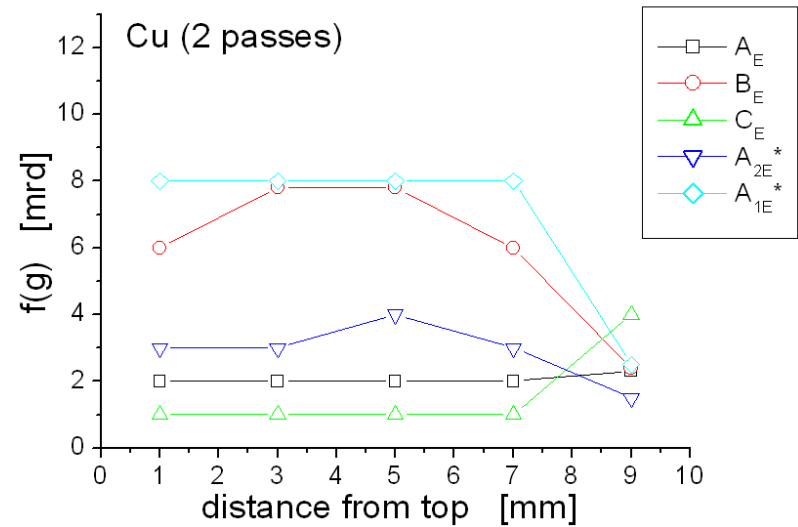
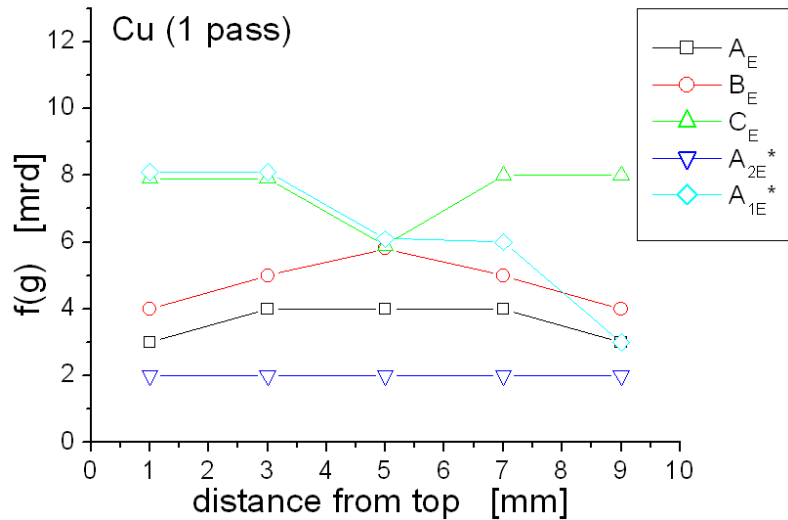
Cu (route A, 1 pass): synchrotron texture



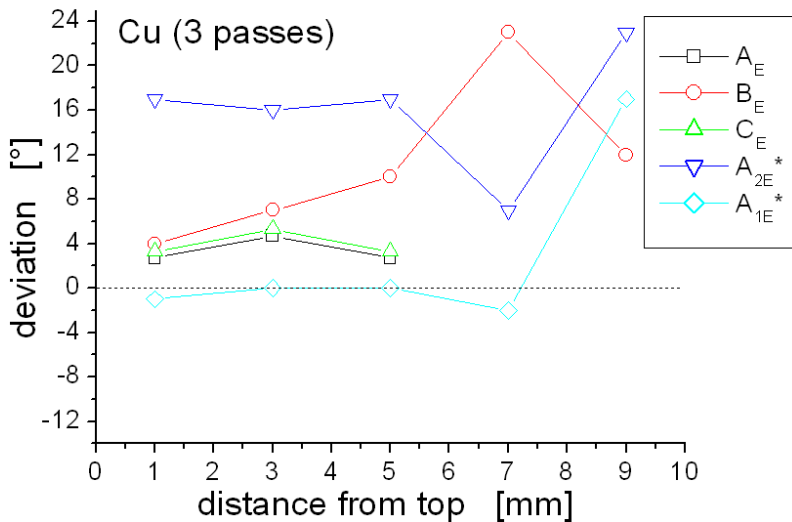
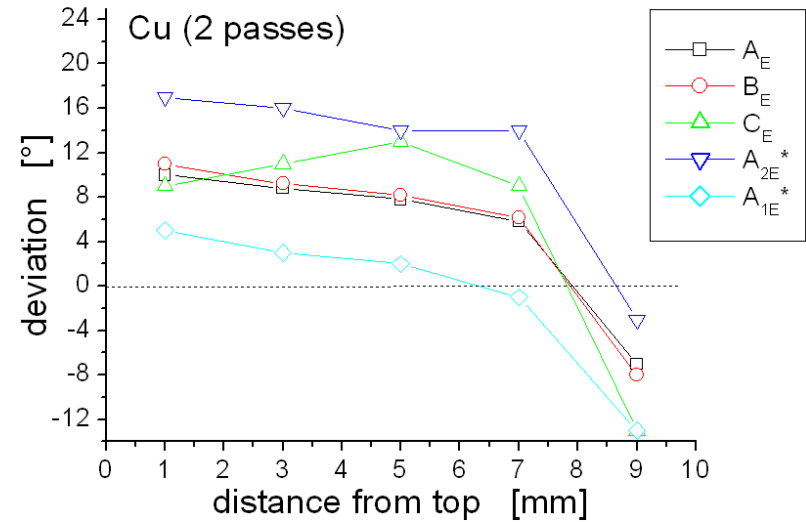
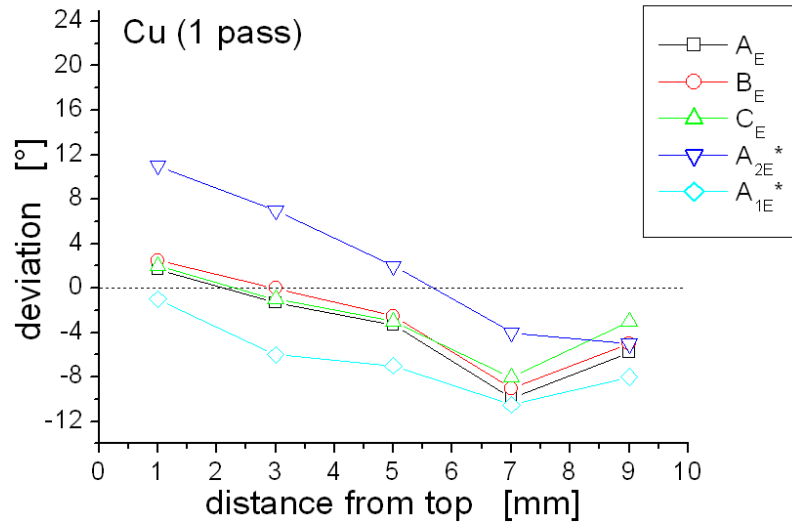
Cu (route A, 3 passes): synchrotron texture



Cu: intensity of texture components

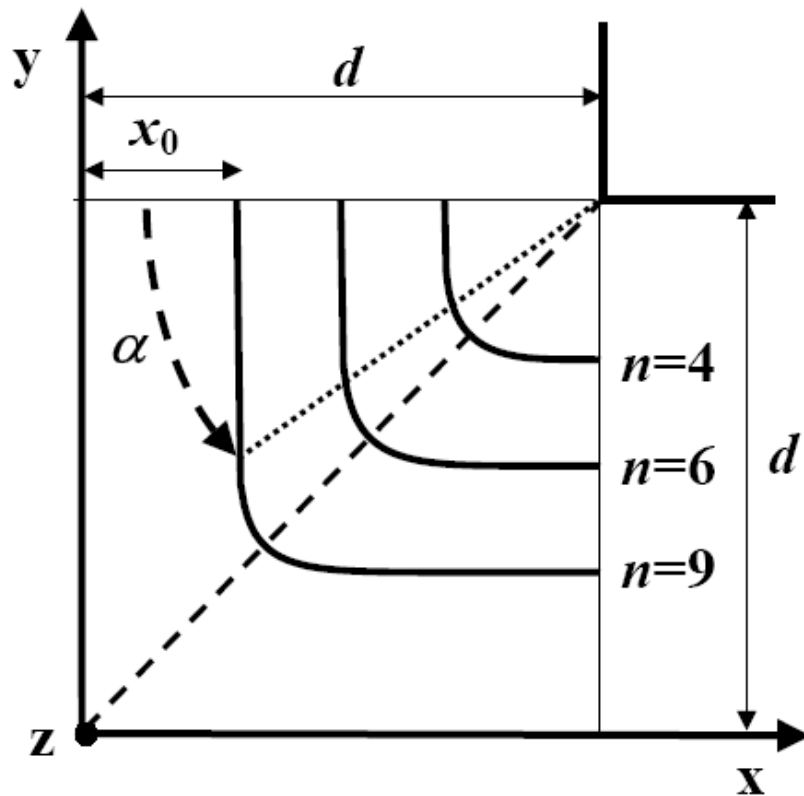


Cu: deviation from ideal components



Negative φ_1 values indicate shift from ideal positions to the left in ODF

Tóth's flow line model of ECAP (I)



$$\phi = (d-x)^n + (d-y)^n = (d-x_0)^n$$

$$v_x = \lambda \frac{\partial \phi}{\partial y}, \quad v_y = -\lambda \frac{\partial \phi}{\partial x}$$

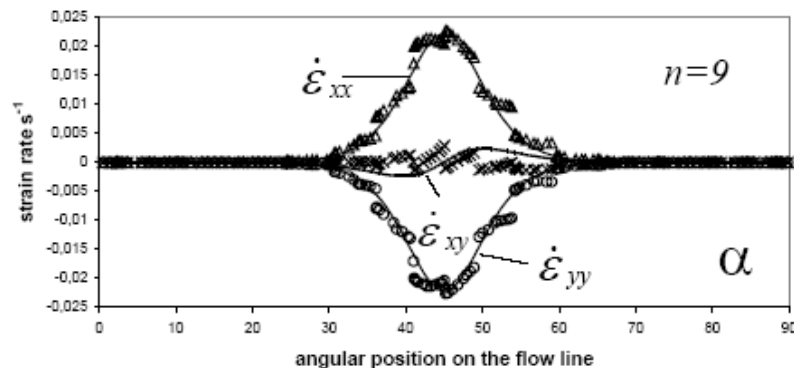
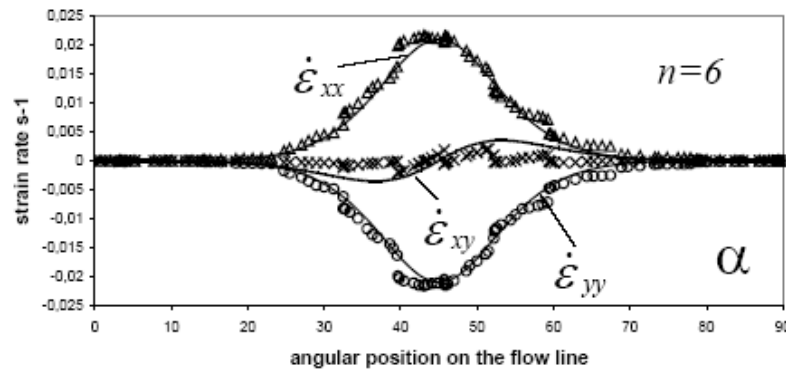
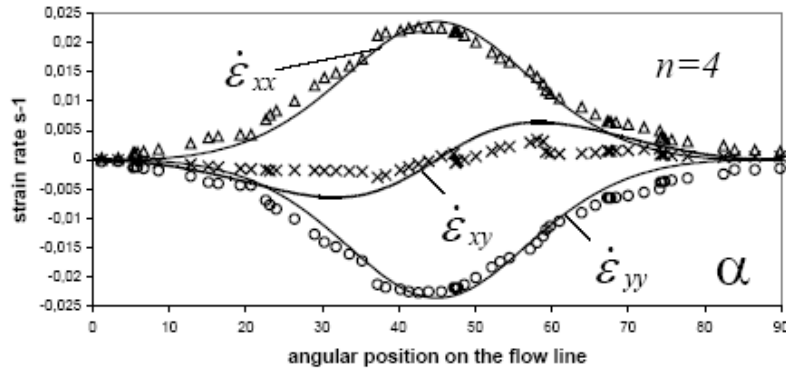
$$v_x = v_0 \left(\frac{d-y}{d-x_0} \right)^{n-1}, \quad v_y = -v_0 \left(\frac{d-x}{d-x_0} \right)^{n-1}$$

$$L_{xx} = \frac{\partial v_x}{\partial x} = -v_0 (1-n) (d-x)^{n-1} (d-y)^{n-1} (d-x_0)^{1-2n},$$

$$L_{yy} = -L_{xx},$$

$$L_{xy} = \frac{\partial v_x}{\partial y} = v_0 (1-n) (d-x)^n (d-y)^{n-2} (d-x_0)^{1-2n},$$

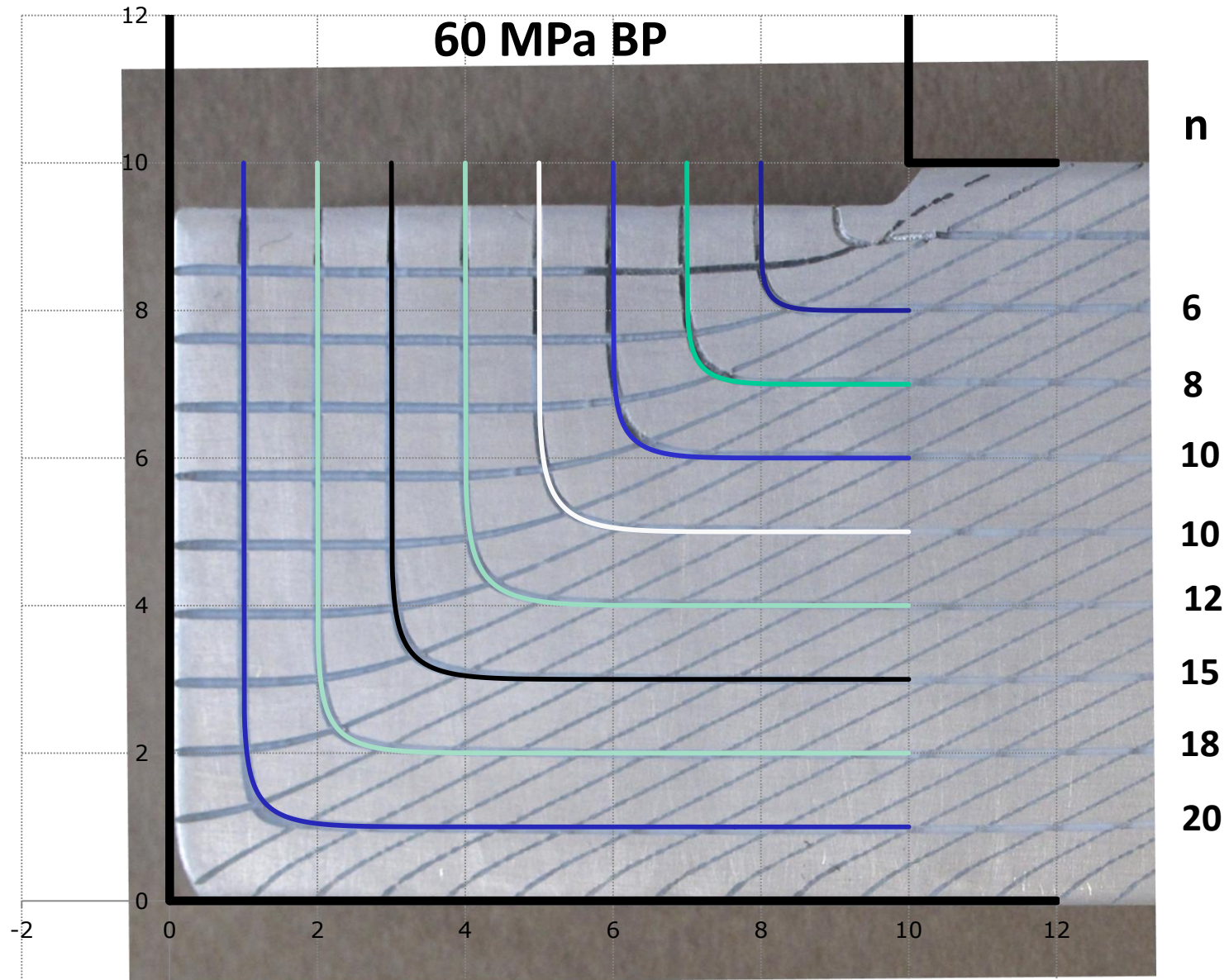
$$L_{yx} = \frac{\partial v_y}{\partial x} = -v_0 (1-n) (d-y)^n (d-x)^{n-2} (d-x_0)^{1-2n}.$$



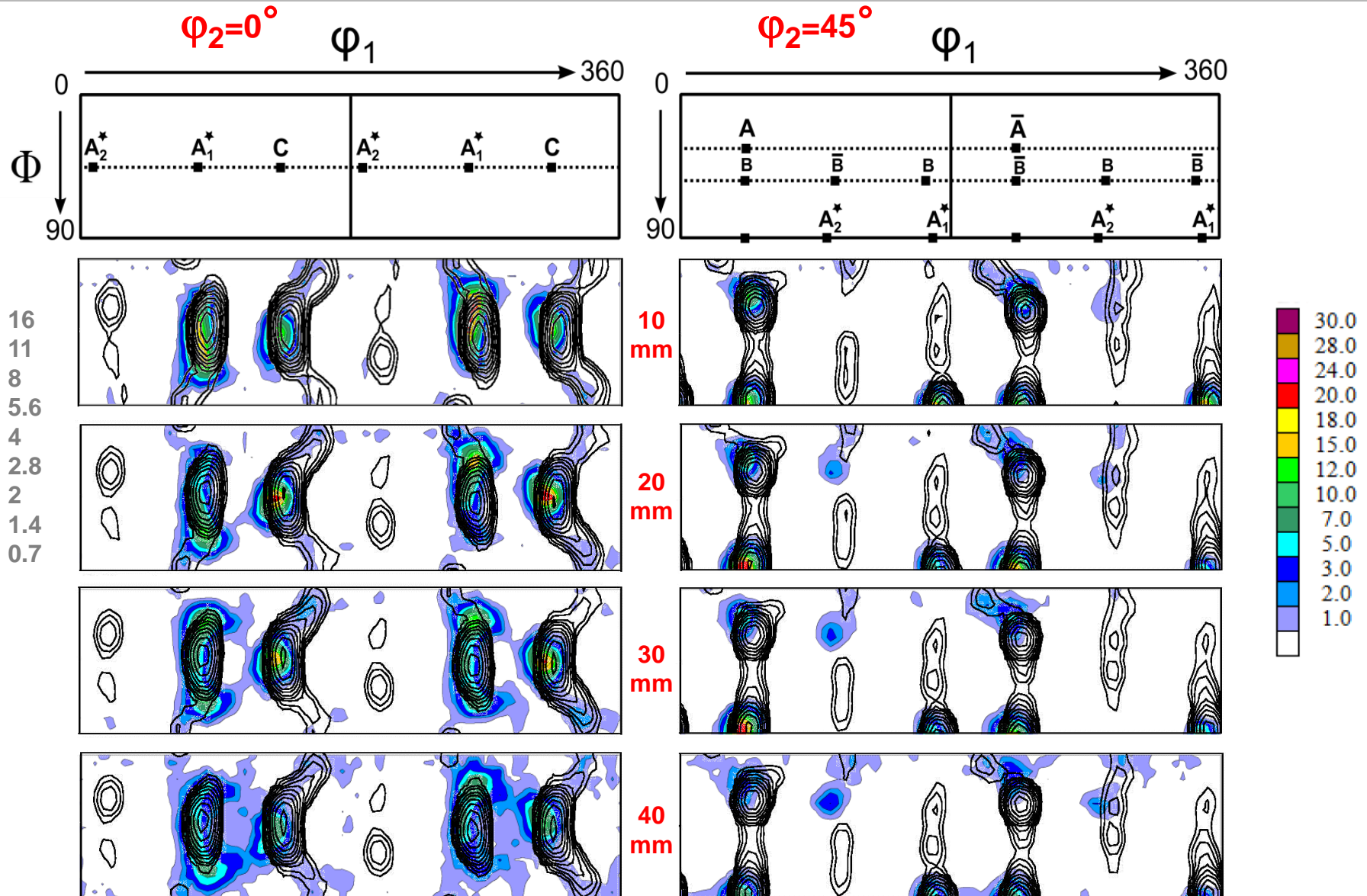
$$\begin{aligned}\dot{\epsilon}_{xx} &= -v_0(1-n)(d-x)^{n-1}(d-y)^{n-1}(d-x_0)^{1-2n}, \\ \dot{\epsilon}_{yy} &= v_0(1-n)(d-x)^{n-1}(d-y)^{n-1}(d-x_0)^{1-2n}, \\ \dot{\epsilon}_{xy} &= \frac{1}{2}v_0(1-n)(d-x_0)^{1-2n} \left[(d-x)^n(d-y)^{n-2} - (d-y)^n(d-x)^{n-2} \right]\end{aligned}$$



Flow line fit

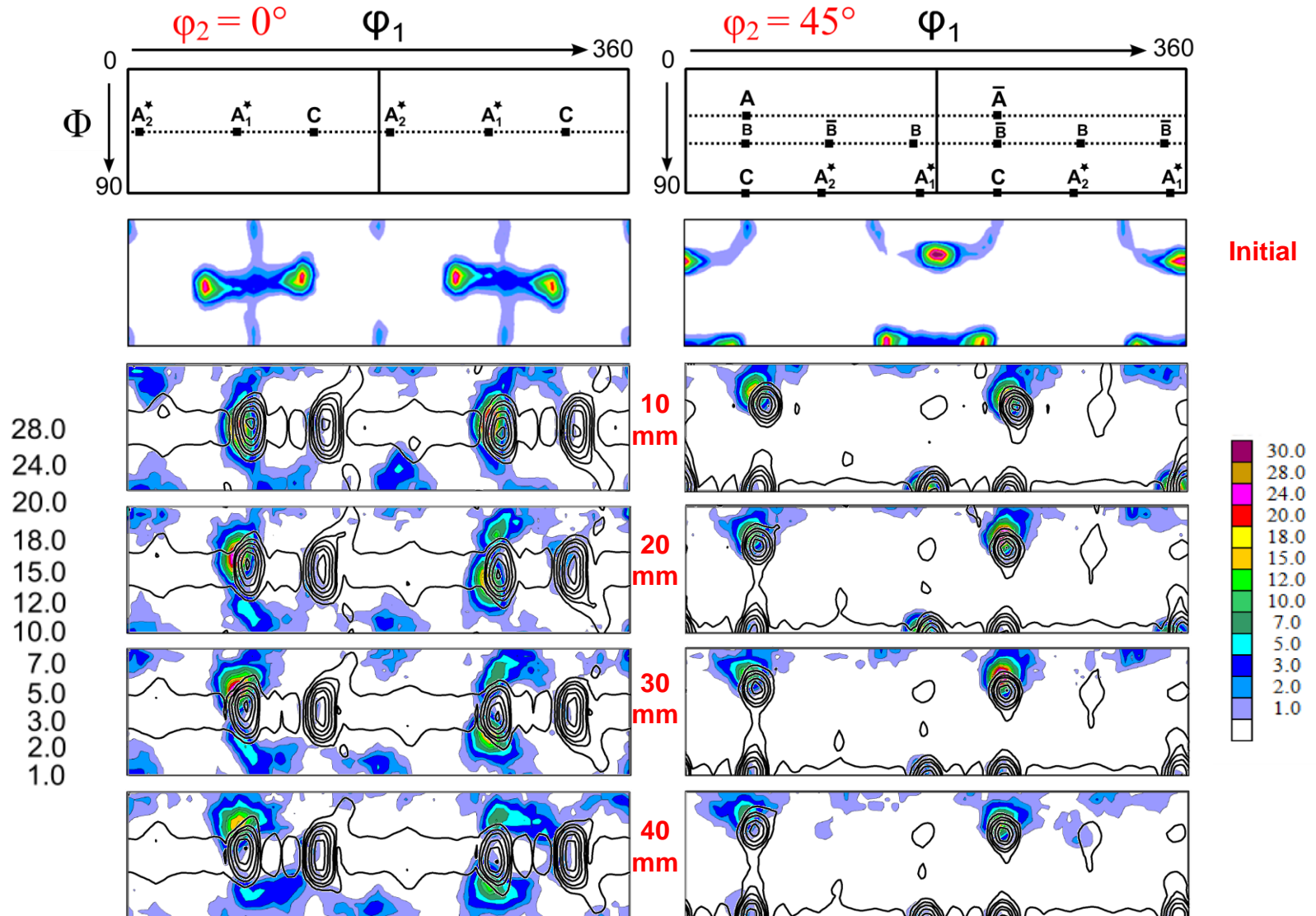


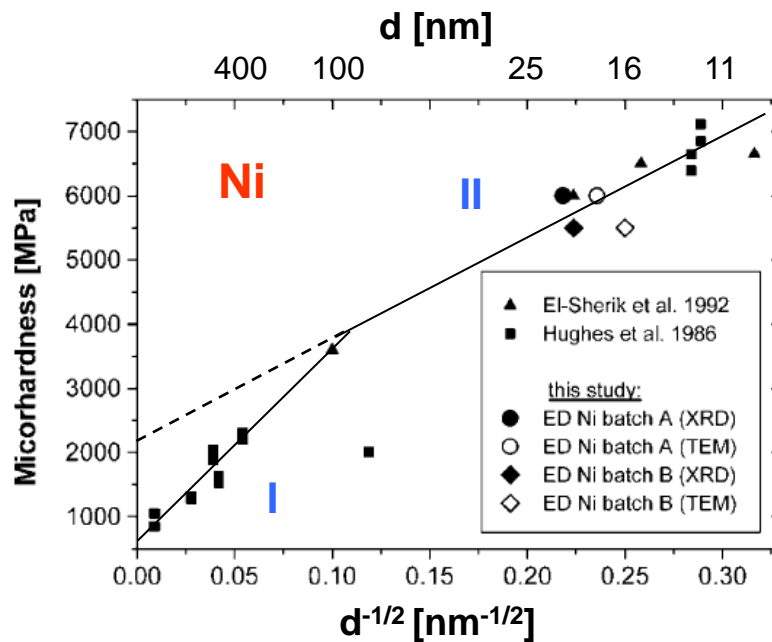
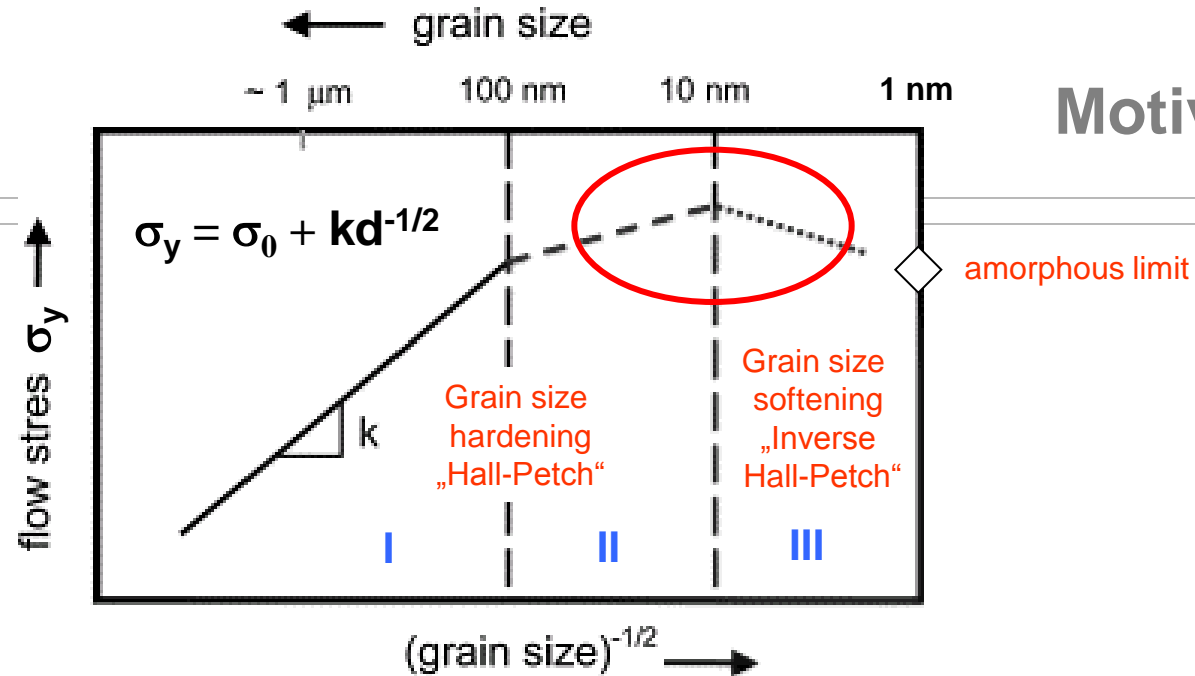
Comparison experiment - simulation 30 MPa BP, oct. + non-oct. slip



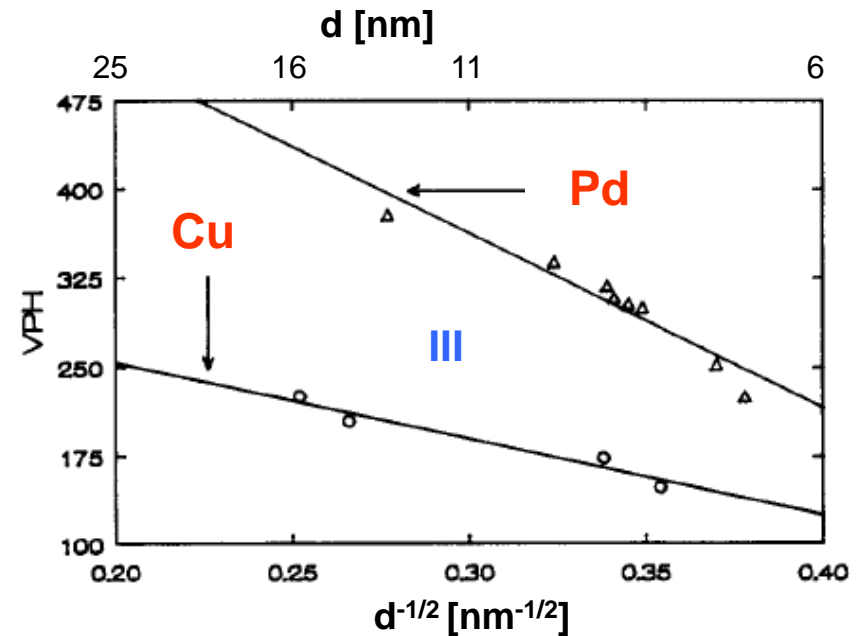
Comparison experiment – simulation

60 MPa BP, oct. + non-oct. slip



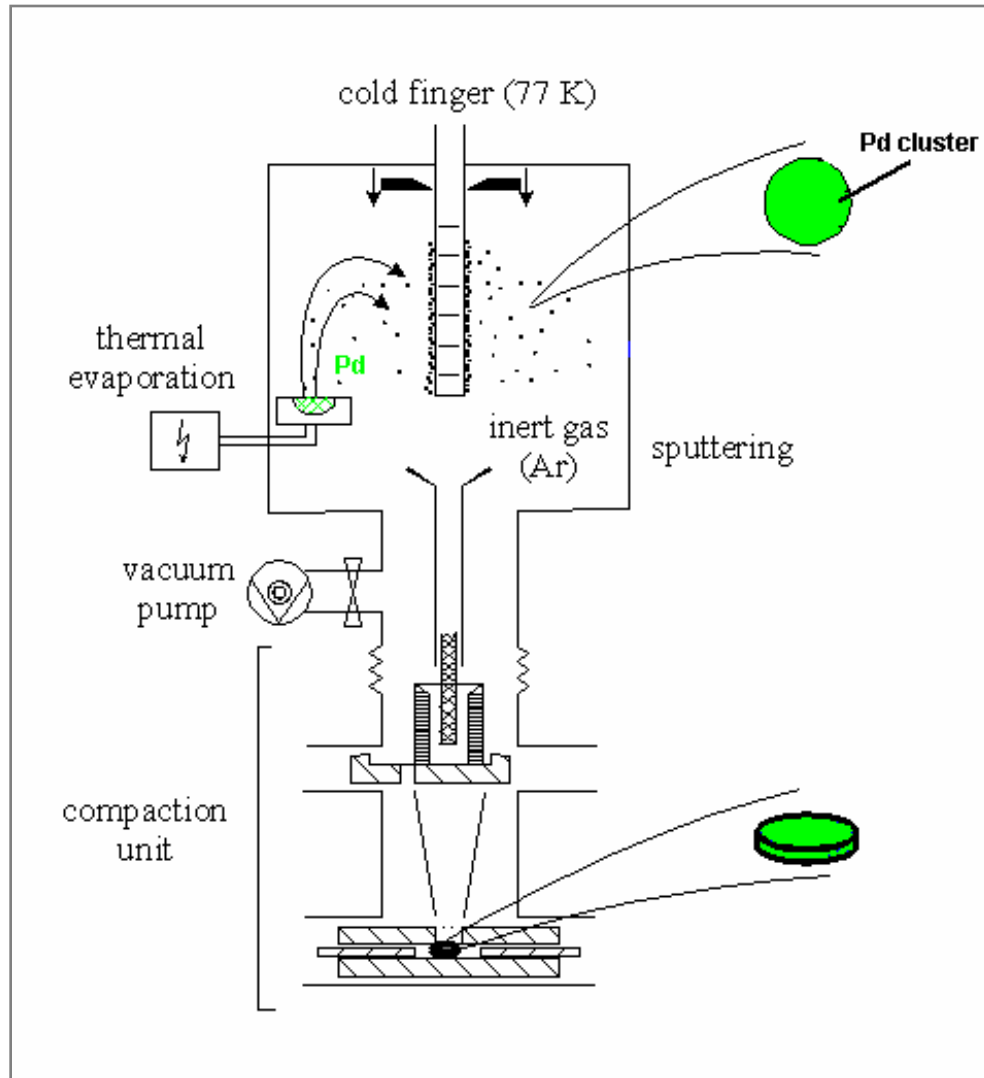


Dalla Torre et al., 2002

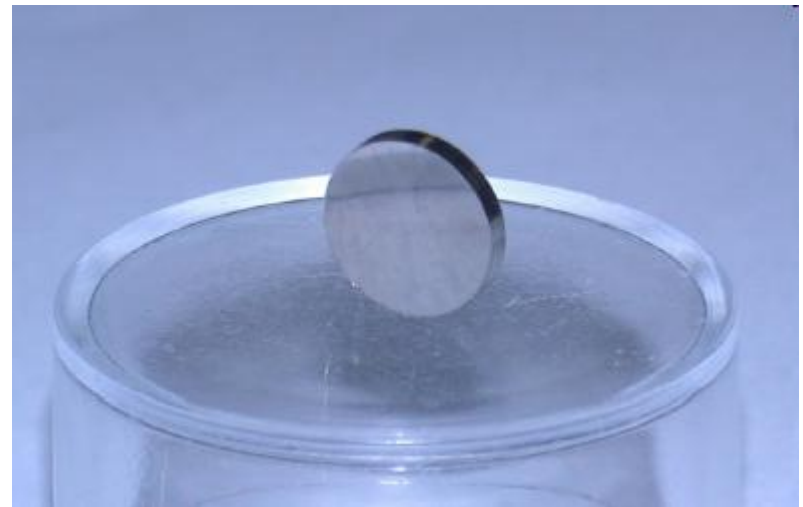


Chokshi et al., 1989

nc sample preparation using inert gas condensation



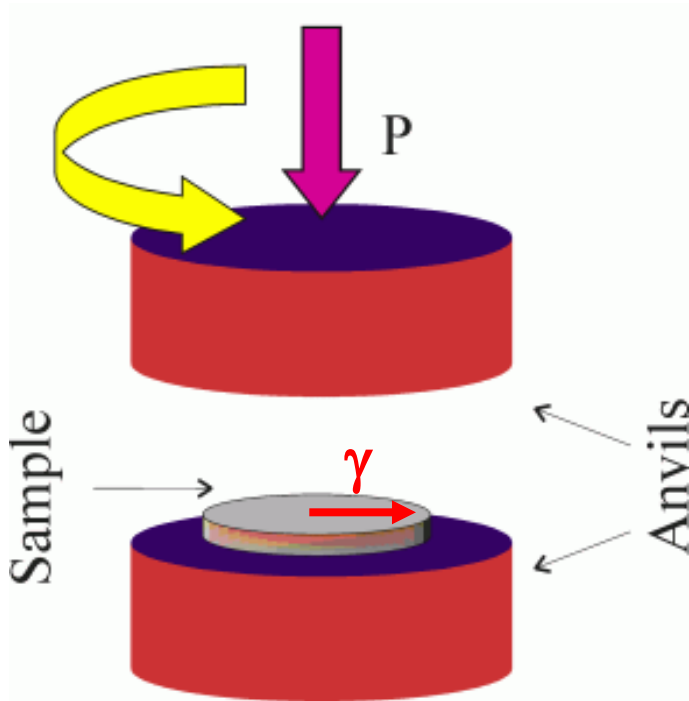
igc pellet



$\varnothing = 8 \text{ mm}$
 $l = 0.3 - 0.5 \text{ mm}$

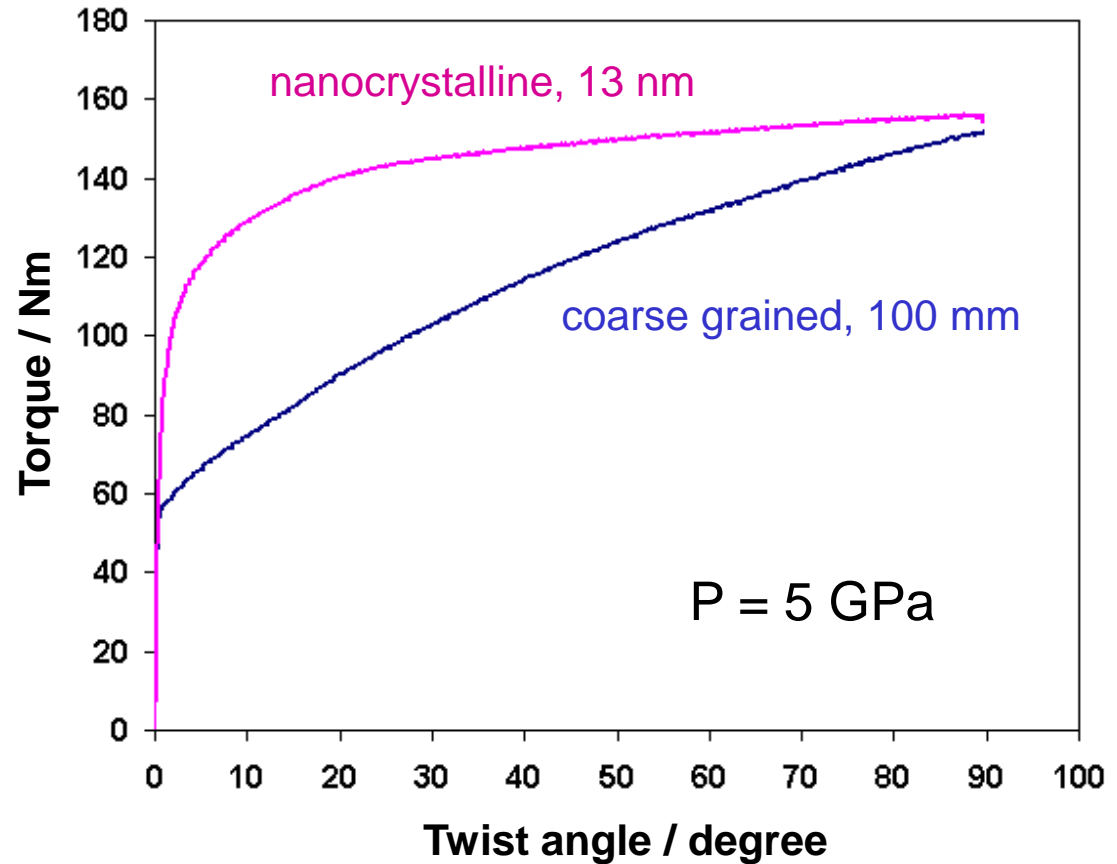
Work in collaboration with Yu. Ivanisenko

High pressure torsion (HPT)



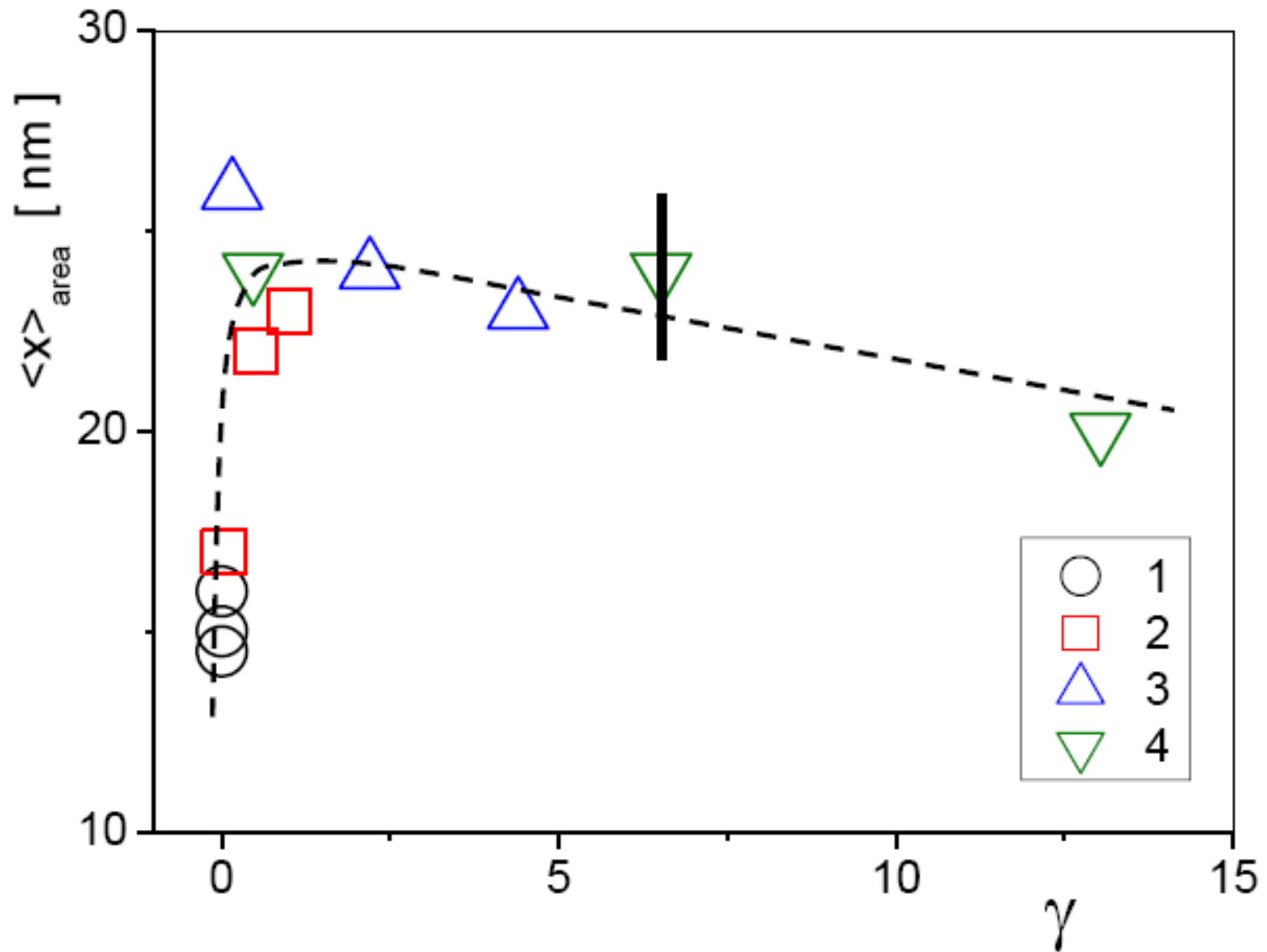
<http://www.ipam.ugatu.ac.ru/spd.html>

Pd-10at.%Au



Work in collaboration with Yu. Ivanisenko

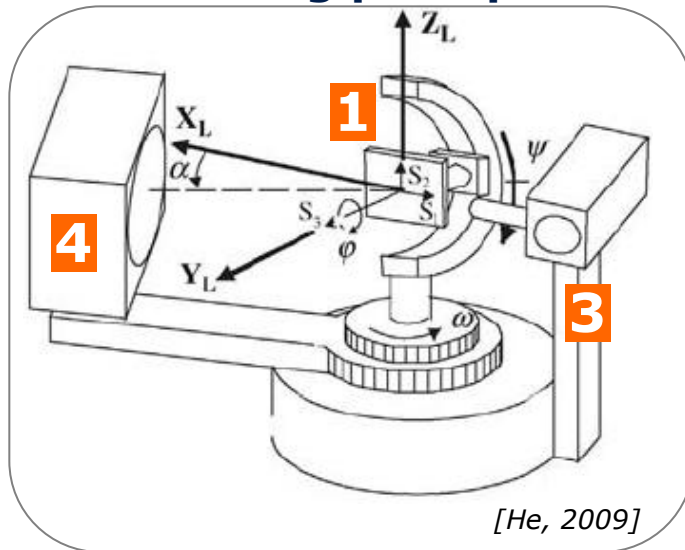
Grain size – shear strain



Microdiffraction by $XR_{\mu}D^2$

Europa fördert Sachsen.
financed by **EFRE**
Europäischer Fonds für
regionale Entwicklung

Measuring principle

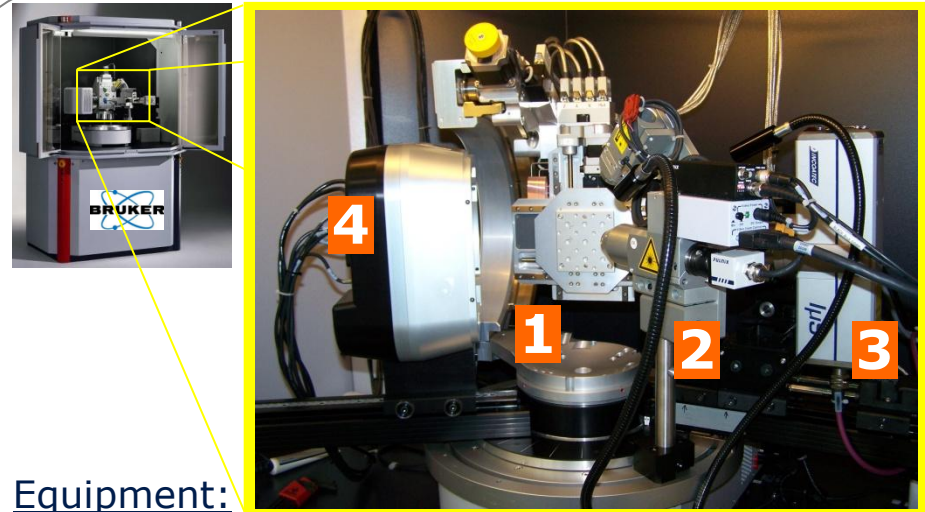


Aims

correlated & spatially resolved

- **texture**
- stress

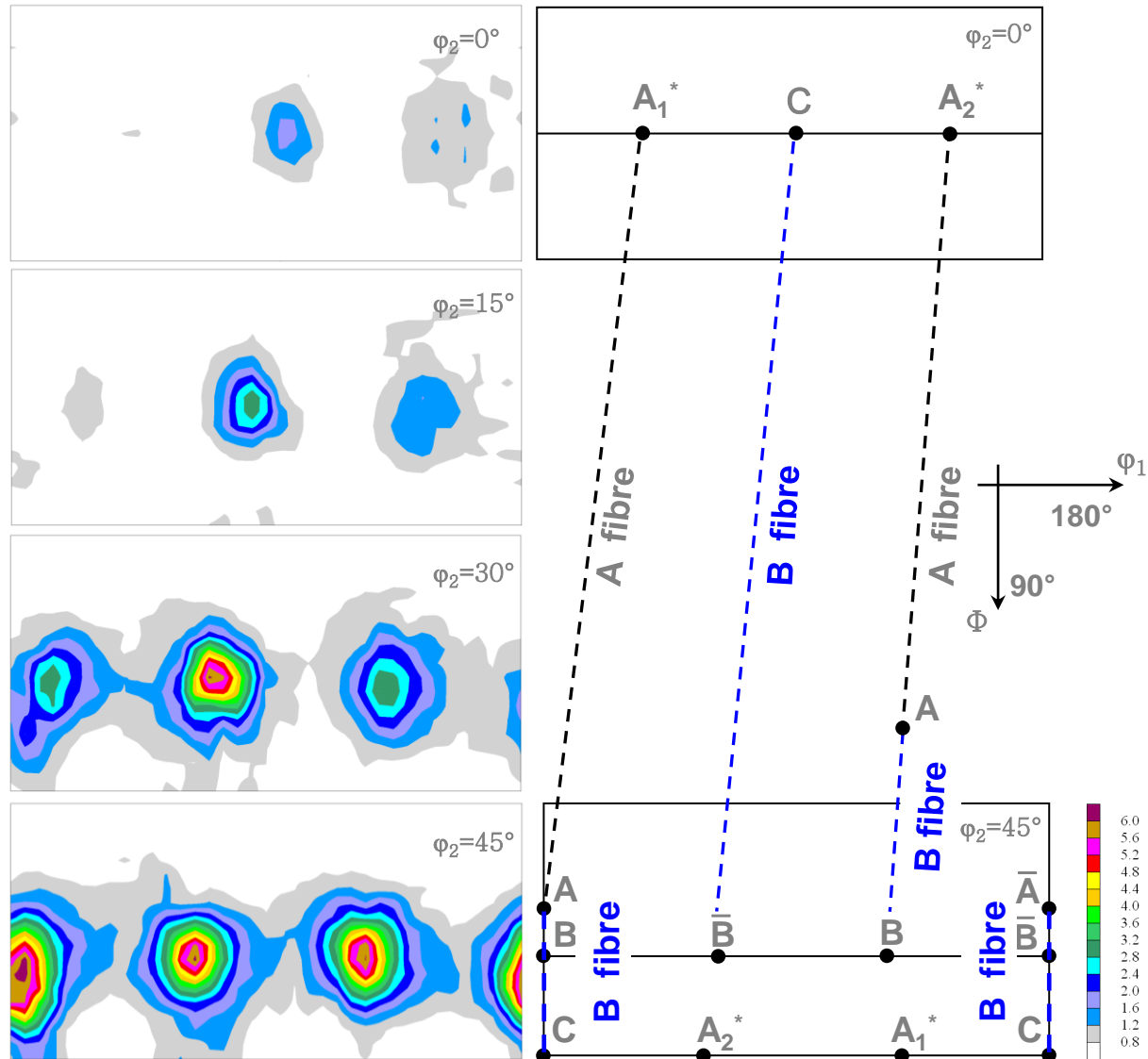
Bruker AXS D8 Discover



Equipment:

- 1** Eulerian cradle with xyz-stage
- 2** Laser-video microscope
- 3** Low-power microfocus X-ray tube $I\mu S$
- 4** 2D detector $V\dot{A}NTEC\ 2000$

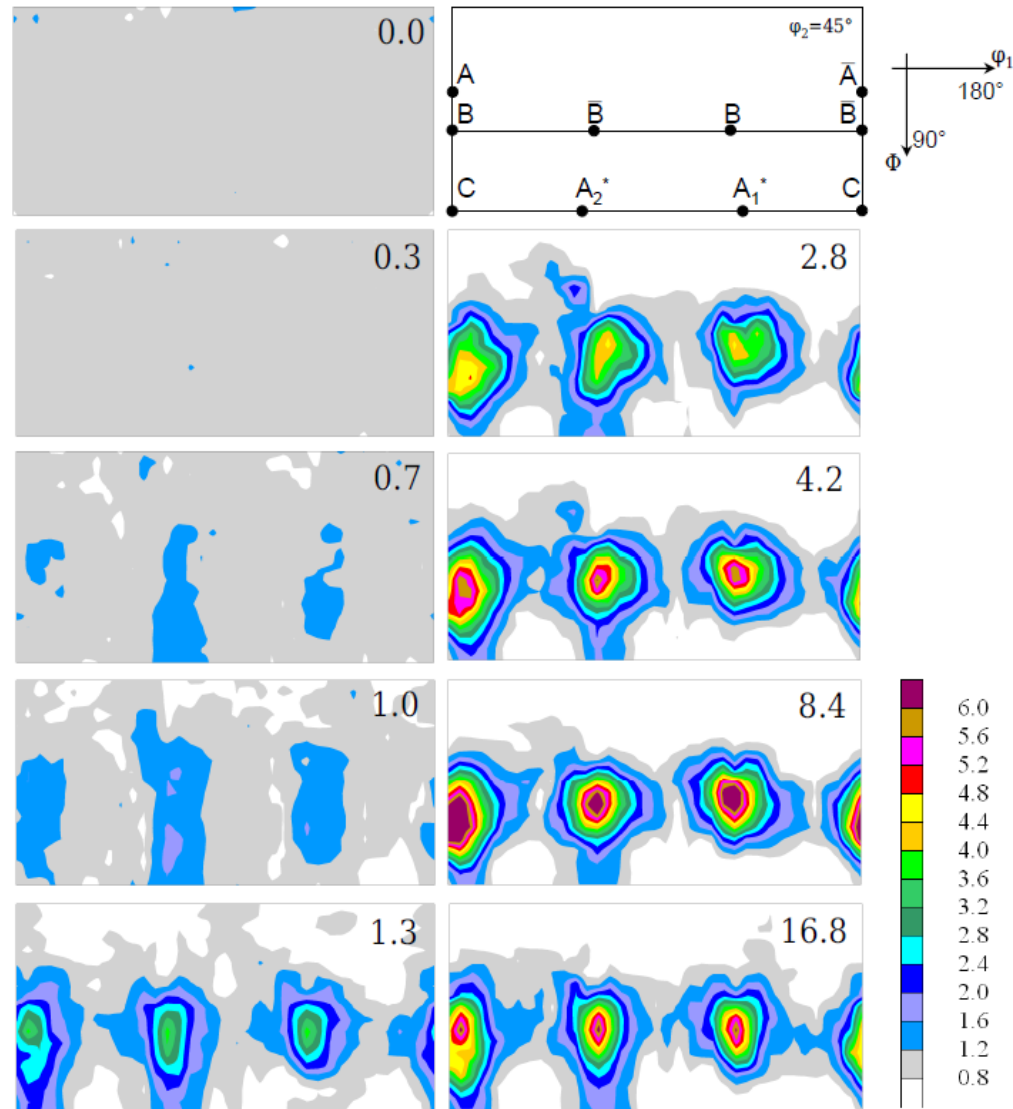
Texture after a shear strain of 12.6

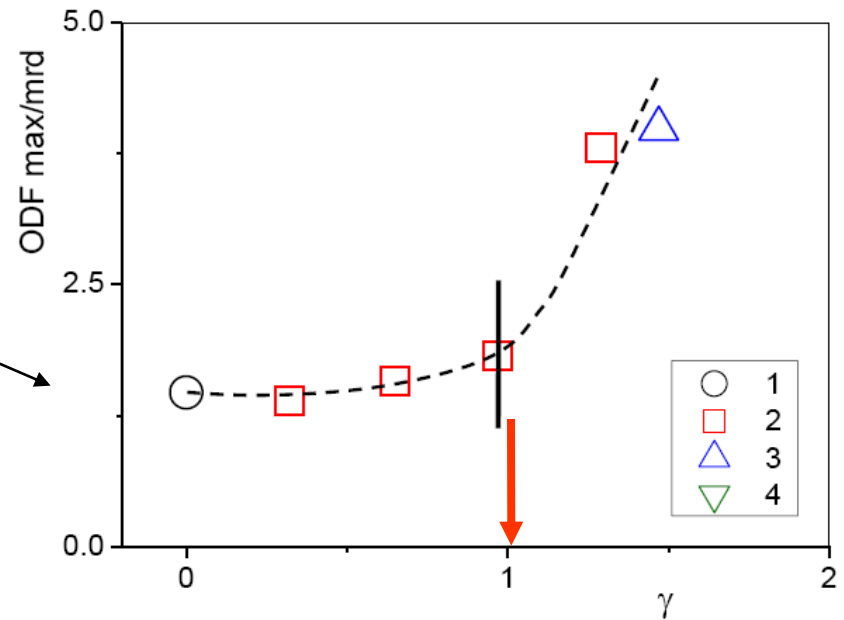
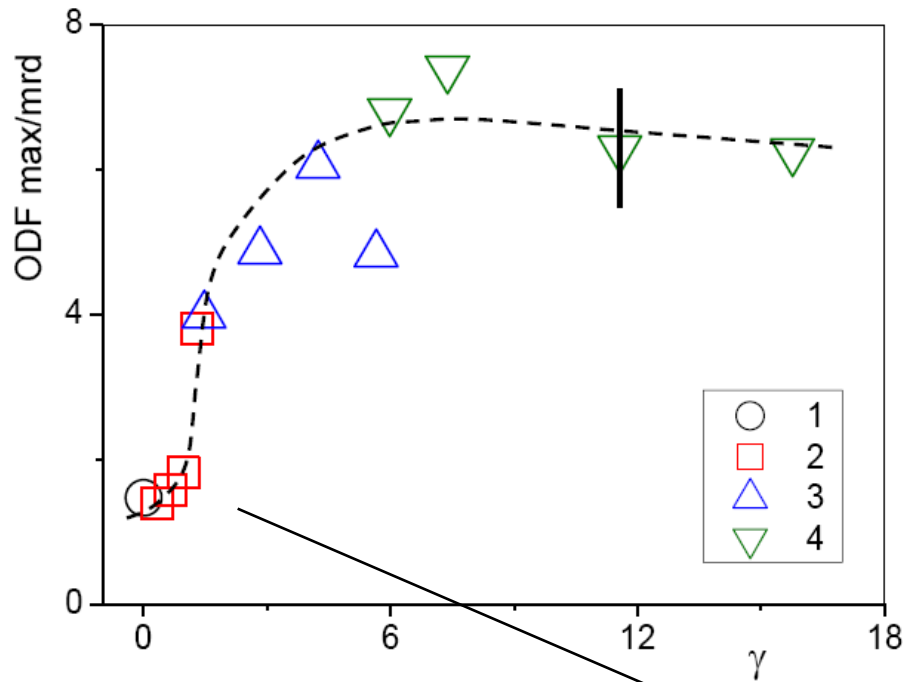


Texture components in simple shear deformed fcc metals

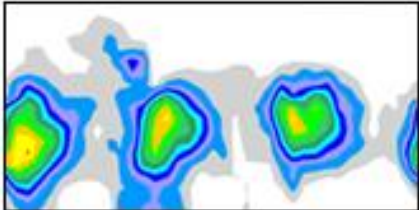
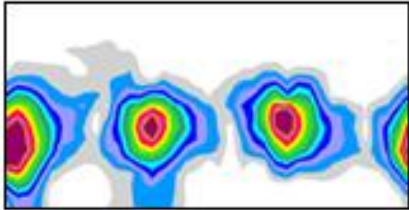
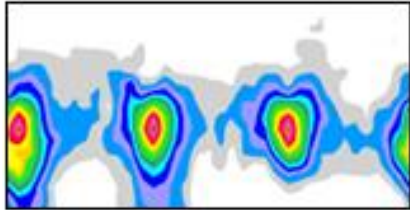
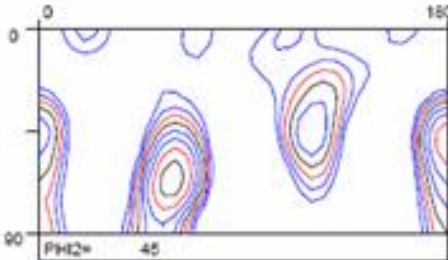
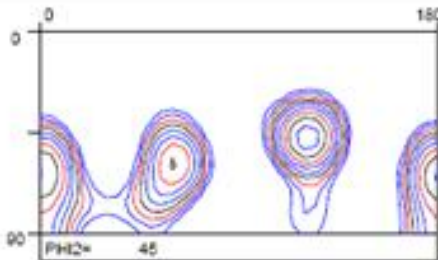
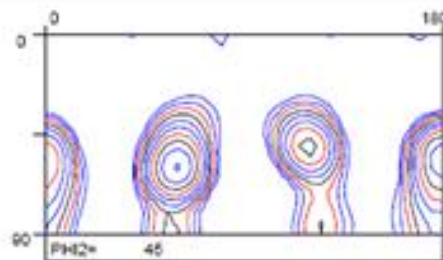
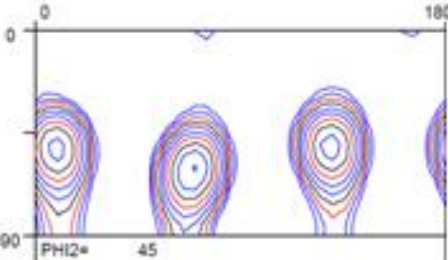
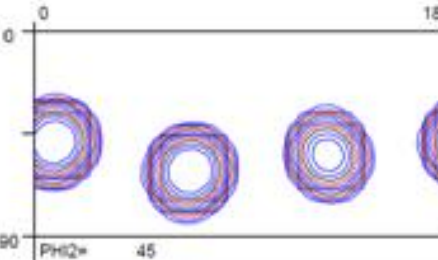
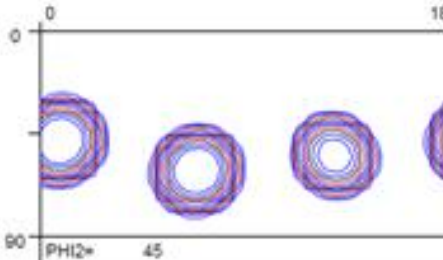
Component designation	Miller indices {shear plane }<shear direction>	Euler angles [°]		
		φ_1	Φ	φ_2
A	$\{1\bar{1}\bar{1}\}<110>$	0	35.26	45
\bar{A}	$\{\bar{1}11\}<\bar{1}\bar{1}0>$	180	35.26	45
A_1^*	$\{\bar{1}\bar{1}1\}<112>$	35.37	45	0
		125.37	90	45
A_2^*	$\{11\bar{1}\}<112>$	144.74	45	0
		54.74	90	45
B	$\{\bar{1}12\}<110>$	0	54.74	45
		120	54.74	45
\bar{B}	$\{1\bar{1}\bar{2}\}<\bar{1}\bar{1}0>$	60	54.74	45
		180	54.74	45
C	$\{001\}<110>$	90	45	0
		0	90	45
$<111>$ or A fibre	$\{111\}<uvw>$			
$<110>$ or B fibre	$\{hkl\}<110>$			

Texture development with shear strain





Modelling of texture development

	$\gamma = 2.83$	$\gamma = 8.38$	$\gamma = 16.76$
Experiment			
Taylor with <110>+<112> CRSS 1.5 : 1			
Taylor with GBS and <110>+<112> CRSS 1.5 : 1			

Contribution of GBS to total strain: 30%

- Choice of radiation, beam size, grain statistics are important for measuring texture gradients.
- Texture gradients in deformed polycrystals are more the rule than the exception.
- Texture gradients lead to gradients in anisotropic properties.
- Texture gradients in torsion deformed samples can be used to show the texture development with shear strain.

Thank you for your kind attention !

Physics Building, Dresden University of Technology



	$d_{1/2}$ [μm] Cu K α ($\lambda = 1,54 \text{ \AA}$)	¹⁰⁴ $d_{1/2}$ [cm] Neutronen ($\lambda = 1,5 \text{ \AA}$)
Pb	2	2,3
Cu	15	0,8
Al	53	6,3
Fe	3	0,5
SiO ₂	76	2,5
CaCO ₃	36	2,1
NaAlSi ₃ O ₈	81	2,5
NaCl	42	0,7
CaSO ₄	32	2,5
PbS	4	3,5
ZnS	24	6,0
Fe ₂ O ₃	6	0,8